## HW-3c: Friction LAB

## ANSWERS

## Background:

Consider a block at rest on a level surface. Imagine trying to pull the box across the surface. The force opposing the pulling force F is the frictional force ( f ).


Figure 1:
N is the normal force of the plane acting on the block, which equals the weight of the block mg , where m is the mass of the block and g is the acceleration due to gravity. $f$ is the resisting force to sliding and F is the applied driving force. At the moment of sliding, the resisting force equals the driving force ( $f=$ $F)$.

Amonton's first law is that the force of friction (f) is directly proportional to the applied load, or:
$f \propto N \quad$ Eq. 1
or
$f=\mu N$
Eq. 2
where $\mu$ is the friction coefficient.
Amonton's second law is that the force of friction is independent of area of contact. At some levels this is self-evident. If we divide equation 2 by the area of contact (A), then
$\frac{f}{A}=\frac{\mu N}{A}$,
Eq. 3
or
$\tau=\mu \sigma_{n}$, Eq. 4
where $\tau$ is the shear stress and $\sigma_{n}$ is the normal stress.

The constant $\mu$ is the coefficient of friction. There are two coefficients of friction to consider in this interaction. The first is the coefficient of static friction $\mu_{s}$. This applies up to the point when the block breaks free and just begins to move. The second is the coefficient of kinetic friction $\mu_{k}$. This applies when the block is sliding along the surface with constant speed (ie. with no acceleration).

When the surface is an inclined plane, the normal force N changes. It is still perpendicular to the plane but the weight of the block is not. The contribution of the weight to N depends on the angle of inclination $\phi$.


Figure 2:
From the diagram, at the point of failure, the frictional force $(f)$ is:
$f=m g \sin \phi$,
Eq. 5
and the normal force $(\mathrm{N})$ is:
$N=m g \cos \phi$.
Eq. 6
Equation 2 can be restated as,
$m g \sin \phi=\mu m g \cos \phi$,
Eq. 7
Or
$\mu=\frac{\sin \phi}{\cos \phi}=\tan \phi$
Eq. 8
The friction coefficient is the slope at which the block begins to slide. So, if we measure the angle of inclination ( $\phi$ ) when the block first breaks free we get $\mu_{\mathrm{s}}$ directly. Likewise, if we measure $(\phi)$ as the block slides with constant speed down the incline we get $\mu_{k}$.

The goal of this lab is to test whether Amonton's $1^{\text {st }}$ law is correct. To do so, we will determine the friction coefficient for one material at a range of normal stresses.

## Procedure:

Materials:

- Hinged wood surface with acrylic and aluminum covers
- Aluminum plate
- Slotted weights
- Spring scale
- Scissor jack
- Support blocks for scissor jack
- Ruler

Place the plate on the right end of the plane (opposite the hinge). Hold the ruler upright at the 50 cm mark on the base and slowly lift the plane to increase the angle. Stop when the plate just breaks free and begins to move.

Measure the height $h$ of the plane; the length I of the base is 50 cm . Calculate the coefficient of static friction.

With this procedure, we measured the following:


Table 1: Experimental results.

1) From these data, calculate the average coefficient of friction and the average friction angle for the experiments with the three different weights. Construct a table. Describe how this supports, or does not support, Amonton's first law.
Amonton's first law is that the force of friction (f) is directly proportional to the applied load, or: $f \propto N$
or
$f=\mu N$
In the experiment we varied the normal force by varying the weight. We showed that the friction coefficient stays constant.

| Mass | Gravitational <br> Accel. $(\mathrm{g})$ <br> $\left(\mathrm{m} / \mathrm{s}^{\wedge} 2\right)$ | Weight <br> $(\mathrm{N})$ | Height <br> $(\mathrm{m})$ | Length <br> $(\mathrm{m})$ | angle of <br> inclination <br> radians | inclination, <br> degrees | friction <br> coefficient |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.32 | 9.8 | 3.14 | 0.195 | 0.5 | 0.37 | 21.3 | 0.39 |


| 0.32 | 9.8 | 3.14 | 0.206 | 0.5 | 0.39 | 22.4 | 0.41 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.32 | 9.8 | 3.14 | 0.212 | 0.5 | 0.40 | 23.0 | 0.42 |
| Average |  |  |  |  | 0.39 | 22.2 | 0.41 |
|  |  |  |  |  |  |  |  |
| 0.47 | 9.8 | 4.61 | 0.215 | 0.5 | 0.41 | 23.3 | 0.43 |
| 0.47 | 9.8 | 4.61 | 0.231 | 0.5 | 0.43 | 24.8 | 0.46 |
| 0.47 | 9.8 | 4.61 | 0.195 | 0.5 | 0.37 | 21.3 | 0.39 |
| Average |  |  |  |  | 0.40 | 23.1 | 0.43 |
|  |  |  |  |  |  |  |  |
| 0.62 | 9.8 | 6.08 | 0.192 | 0.5 | 0.37 | 21.0 | 0.38 |
| 0.62 | 9.8 | 6.08 | 0.181 | 0.5 | 0.35 | 19.9 | 0.36 |
| 0.62 | 9.8 | 6.08 | 0.184 | 0.5 | 0.35 | 20.2 | 0.37 |
| Average |  |  |  |  | 0.36 | 20.4 | 0.37 |

Table 2: Analysis of Experimental results.
2) Construct a Mohr diagram illustrating the stress state for each of the three experiments. To construct this diagram, I found it helpful to remember the following. First, a Mohr diagram is in stress, not pressure. I assumed a unit area (A). Thus, I really just plotted the forces, but I envisioned that they were divided by an area equal to unity. Second, I drew out the geometric relationships so that I could calculate the center point of the Mohr Circle (the average stress) and the radius of the Mohr's circle. These are illustrated in my pencil sketch below.


Figure 3: The relationship between friction angle ( $\phi$ ), the normal stress on the failure plane ( $N / A$ ), shear stress along the failure plane (T/A), and the center of the Mohr's circle ((N/A)+b), and the radius of the Mohr's circle (r).


Figure 4:

|  | phi-radians | N/A | T/A | sigma- <br> av | r | sigma1 | sigma3 | 45+phi/2 | 45-phi/2 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| exp. 1 | 0.39 | 2.9 | 1.2 | 3.4 | 1.3 | 4.7 | 2.1 | 56.1 | 33.9 |
| exp. 2 | 0.40 | 4.2 | 1.8 | 5.0 | 2.0 | 7.0 | 3.0 | 56.6 | 33.4 |
| exp. 3 | 0.36 | 5.7 | 2.1 | 6.5 | 2.3 | 8.7 | 4.2 | 55.2 | 34.8 |

Table 3: Plotting Mohr circles for experiment. A=Area $=1 m^{\wedge} 2$, $r=$ radius of Mohr's Circle (maximum shear stress), $N / A=$ normal stress along failure plane, $T / A=$ Shear stress along failure plane, sigma $1=$ max. principal stress, sigma $3=$ least principal stress

Please construct a table that shows the average stress and the maximum shear stress for each stress state. On your diagram, label the stress points where failure occurs. Make sure you plot your inferred failure surface. Make sure you plot the Mohr circle for each experiment on the diagram.
3) Imagine that you are in a normal faulting situation. What is the dip angle at which a fault will form. Imagine you are in a compressional (thrust fault) setting. What is the dip angle at which faults will form?

$$
\theta_{c r}=45+\frac{\phi^{\prime}}{2}
$$

$\theta$ is the angle relative to plane normal to the maximum principal stress. In a normal faulting situation, we assume $\sigma_{1}$ is vertical. Thus, the dip angle is $\sim 56$ degrees (Table 3 ). In a thrust faulting environment, $\sigma_{1}$ is horizontal. Thus, the dip angle (the angle from the horizontal plane) is actually $\theta_{c r}=45-\frac{\phi^{\prime}}{2}$, or approximately 34 degrees (table 1 ).
4) Please construct an 'average stress' vs. 'maximum shear stress' plot for each of the three stress points. Please label the failure line such that the failure line intersects with the average stress points.


Figure 5: Average stress (s) vs. maximum shear stress (t) for the three experiments. I have drawn the failure surface $\left(t_{f}=s * \sin (\phi)\right)$ assuming a friction angle of 23.1 degrees.

